

Reports of the Department of Geodetic Science  
Report No. 184

# **COORDINATE TRANSFORMATION BY MINIMIZING CORRELATIONS BETWEEN PARAMETERS**

by  
Muneendra Kumar

Prepared for  
National Aeronautics and Space Administration  
Washington, D. C.

Contract No. NGR 36-008-093  
OSURF Project No. 2514



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The Ohio State University  
Research Foundation  
Columbus, Ohio 43212

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## PREFACE

This project is under the supervision of Ivan I. Mueller, Professor of the Department of Geodetic Science at The Ohio State University, and is under the technical direction of James P. Murphy, Special Programs, Code ES, NASA Headquarters, Washington, D. C. The contract is administered by the Office of University Affairs, NASA, Washington, D. C. 20546

A revised version of this report has been submitted to the Graduate School of The Ohio State University in partial fulfillment of the requirements for the Master of Science degree.

## ABSTRACT

The subject of this investigation is to determine the transformation parameters (three rotations, three translations and a scale factor) between two Cartesian coordinate systems from sets of coordinates given in both systems. The objective is the determination of well separated transformation parameters with reduced correlations between each other, a problem especially relevant when the sets of coordinates are not well distributed. The above objective is achieved by preliminarily determining the three rotational parameters and the scale factor from the respective direction cosines and chord distances (these being independent of the translation parameters) between the common points, and then computing all the seven parameters from a solution in which the rotations and the scale factor are entered as weighted constraints according to their variances and covariances obtained in the preliminary solutions.

Numerical tests involving two geodetic reference systems were performed to evaluate the effectiveness of this approach as follows:

- (a) A non-constrained solution for general transformation for the seven parameters (including the three translations and scale factor).
- (b) A constrained solution for general transformation for the seven parameters utilizing the three rotations with their statistics as constraints.
- (c) A constrained solution for general transformation for the seven parameters using the three rotations and scale factor with their statistics as constraints.

The above schemes were then separately repeated for each of the following three cases:

- (i) Using the full variance-covariance matrix between coordinates of the geodetic reference systems.
- (ii) Using only a  $(3 \times 3)$  banded diagonal variance-covariance matrix, thus assuming no correlation between coordinates of any two points within the system.
- (iii) Using only variances for the coordinates, thereby further omitting the correlation between the three coordinates of any one point in the system.

In the case of seven parameter general transformation, the best estimates were obtained using full variance-covariance matrix and constraining three rotations and the scale factor, case (c) and (iii) above. The improvement in correlation between translations and rotations was more significant compared to between translation and scale factor.

## ACKNOWLEDGMENTS

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## 1. INTRODUCTION

During the last twenty-five years with the availability of computer technology and its phenomenal growth in basic hardware and core storage capacity and the exceptional increase in a computer's ability of solving problems in lesser and lesser time, a trend has set in to analyze the problems in geodesy and photogrammetry more and more in three dimensional space rather than to follow traditional concepts.

Further, the advent of artificial satellites and their subsequent use in geodesy made it possible to obtain Cartesian coordinates of points on earth surface.

Several projects involving satellite-networks of continental or global extent were begun and at present they are in varying stages of completion. Many new solutions have recently come out, each delineating its own reference system. These systems in reality should differ from each other only in having different origins, sets of axes or scale.

Thus, the relationship between any two such reference systems (e. g., UVW and XYZ) would generally consist of seven parameters—three translations ( $\Delta X, \Delta Y, \Delta Z$ ) between the two origins, three rotations ( $\omega, \psi, \epsilon$ ) of the Euler's angle type between the two sets of axes and the scale factor ( $\Delta s$ ), if any (Figure 1).

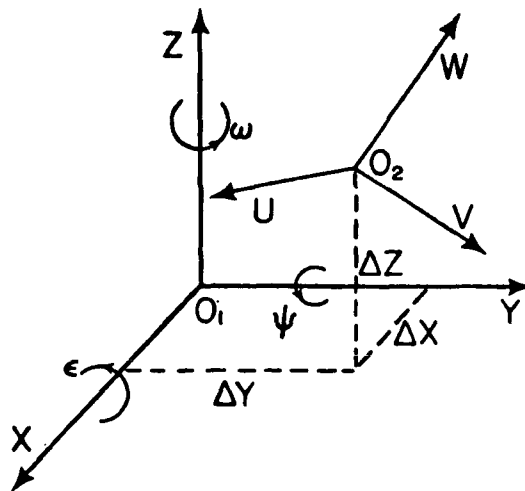


Figure 1.

The mathematical model to be used in the computations of the above seven parameters from a least squares solution may be written in the following form [Badekas, 1969; Bursa, 1965; Wolf, 1963]:

$$\begin{bmatrix} f_1 \\ f_2 \\ f_3 \end{bmatrix} \equiv \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_i - \begin{bmatrix} \Delta X \\ \Delta Y \\ \Delta Z \end{bmatrix}_i - \begin{bmatrix} 1 & \omega & -\psi \\ -\omega & 1 & \epsilon \\ \psi & -\epsilon & 1 \end{bmatrix} \begin{bmatrix} U \\ V \\ W \end{bmatrix}_i - \Delta s \begin{bmatrix} U \\ V \\ W \end{bmatrix}_i = 0, \quad (1)$$

where "i" denotes any point common to both the systems. The three angles  $\omega$ ,  $\psi$ , and  $\epsilon$  of the Euler type correspond to small rotations about the Z, Y and X axes respectively—the positive direction of rotations taken in counter clockwise mode, when viewed from the end of the respective axes towards the origin. It may be worth while to mention here that the station coordinates in both the systems ( $U_1, V_1, W_1$  and  $X_1, Y_1, Z_1$ ) are treated as observations in the above model.

The above equation written in matrix notation can then be modified into the observation equation below [Uotila, 1967]:

$$BV + AX + W = 0, \quad (2)$$

where

$$B \equiv \begin{bmatrix} \frac{\partial f_1}{\partial X} & \frac{\partial f_1}{\partial Y} & \frac{\partial f_1}{\partial Z} & \frac{\partial f_1}{\partial U} & \frac{\partial f_1}{\partial V} & \frac{\partial f_1}{\partial W} \\ \frac{\partial f_2}{\partial X} & \frac{\partial f_2}{\partial Y} & \frac{\partial f_2}{\partial Z} & \frac{\partial f_2}{\partial U} & \frac{\partial f_2}{\partial V} & \frac{\partial f_2}{\partial W} \\ \frac{\partial f_3}{\partial X} & \frac{\partial f_3}{\partial Y} & \frac{\partial f_3}{\partial Z} & \frac{\partial f_3}{\partial U} & \frac{\partial f_3}{\partial V} & \frac{\partial f_3}{\partial W} \end{bmatrix}_i$$

$$= \begin{bmatrix} 1 & 0 & 0 & -1 & 0 & 0 \\ 0 & 1 & 0 & 0 & -1 & 0 \\ 0 & 0 & 1 & 0 & 0 & -1 \end{bmatrix},$$

$$A \equiv \begin{bmatrix} \frac{\partial f_1}{\partial \Delta X} & \frac{\partial f_1}{\partial \Delta Y} & \frac{\partial f_1}{\partial \Delta Z} & \frac{\partial f_1}{\partial \Delta s} & \frac{\partial f_1}{\partial \omega} & \frac{\partial f_1}{\partial \psi} & \frac{\partial f_1}{\partial \epsilon} \\ \frac{\partial f_2}{\partial \Delta X} & \frac{\partial f_2}{\partial \Delta Y} & \frac{\partial f_2}{\partial \Delta Z} & \frac{\partial f_2}{\partial \Delta s} & \frac{\partial f_2}{\partial \omega} & \frac{\partial f_2}{\partial \psi} & \frac{\partial f_2}{\partial \epsilon} \\ \frac{\partial f_3}{\partial \Delta X} & \frac{\partial f_3}{\partial \Delta Y} & \frac{\partial f_3}{\partial \Delta Z} & \frac{\partial f_3}{\partial \Delta s} & \frac{\partial f_3}{\partial \omega} & \frac{\partial f_3}{\partial \psi} & \frac{\partial f_3}{\partial \epsilon} \end{bmatrix}_i$$

$$= \begin{bmatrix} -1 & 0 & 0 & -U & -V & W & 0 \\ 0 & -1 & 0 & -V & U & 0 & -W \\ 0 & 0 & -1 & -W & 0 & -U & V \end{bmatrix}_i ,$$

$$W = \begin{bmatrix} X - U \\ Y - V \\ Z - W \end{bmatrix}_i ,$$

while V and X represent the residuals to the observations and corrections to the parameter estimates, respectively. Hence, collecting all the matrices as above, pointwise in the systems, the observation equation becomes:

$$\begin{bmatrix} 1 & 0 & 0 & -1 & 0 & 0 \\ 0 & 1 & 0 & 0 & -1 & 0 \\ 0 & 0 & 1 & 0 & 0 & -1 \end{bmatrix} \begin{bmatrix} V_x \\ V_y \\ V_z \\ V_u \\ V_v \\ V_w \end{bmatrix}_i + \begin{bmatrix} -1 & 0 & 0 & -U & -V & W & 0 \\ 0 & -1 & 0 & -V & U & 0 & -W \\ 0 & 0 & -1 & -W & 0 & -U & V \end{bmatrix}_i \begin{bmatrix} \Delta X \\ \Delta Y \\ \Delta Z \\ \Delta s \\ \omega \\ \psi \\ \epsilon \end{bmatrix} + \begin{bmatrix} X - U \\ Y - V \\ Z - W \end{bmatrix}_i = 0 \quad (3)$$

Defining the geodetic reference systems on the assumption that the Laplace-condition has been enforced throughout the network (which implies that the axes of the reference ellipsoid are parallel to the conventional earth-fixed axes), many experiments have been made in recent times to determine the seven transformation parameters in relating the different geodetic systems to each other using an observation equation of type (3) [Lambeck, 1971; Marsh et.al., 1971].

However, in the above general transformation, if the geodetic reference systems are properly oriented through the Laplace-condition, the three rotations arising due to the improper relative orientation of the systems are generally never more than a few seconds of arc, while translations may amount up to 200 to 300 meters. Also, due to the presence of high correlations between the rotations, the scale factor and the translations, satisfactory independent estimates for these parameters are difficult to obtain from a combined general solution using equation (3).

This investigation separates the determinations of the rotations and the scale factor (from that of the translations) for subsequent use as constraints in a combined general solution.

## 2. THE INDEPENDENT DETERMINATIONS OF ROTATIONAL AND SCALAR PARAMETERS

### 2.1 Determination of Rotations

#### 2.1.1 Mathematical Model

The mathematical model used in this study is as follows [Bursa, 1966]:

$$\begin{aligned} T_{ik}^{(1)} - T_{ik}^{(2)} + \omega + \psi \sin T_{ik}^{(1)} \tan \delta_{ik}^{(1)} - \epsilon \cos T_{ik}^{(1)} \tan \delta_{ik}^{(1)} &= 0 \\ \delta_{ik}^{(1)} - \delta_{ik}^{(2)} + \psi \cos T_{ik}^{(1)} + \epsilon \sin T_{ik}^{(1)} &= 0 \end{aligned} \tag{4}$$

where  $T_{ik}$  and  $\delta_{ik}$  are defined as the geodetic hour angle and declination of the  $(i-k)^{th}$  direction of the observed point at  $k^{th}$  station and the observer at  $i^{th}$  station. The indexes (1) and (2) denote the two systems with the transformation proceeding from system #1 to system #2.

If  $A_{ik}$ ,  $B_{ik}$ ,  $C_{ik}$  are taken to denote the direction cosines of the  $(i-k)^{th}$  line of length  $R_{ik}$ , then for the first (UVW) system one gets:

$$\begin{aligned}
A_{ik} &= \frac{U_k - U_i}{R_{ik}} = \frac{\Delta U_{ik}}{R_{ik}}, \\
B_{ik} &= \frac{V_k - V_i}{R_{ik}} = \frac{\Delta V_{ik}}{R_{ik}}, \\
C_{ik} &= \frac{W_k - W_i}{R_{ik}} = \frac{\Delta W_{ik}}{R_{ik}},
\end{aligned}
\tag{5}$$

$$\begin{aligned}
\text{and } T_{ik} &= -\arctan \frac{B_{ik}}{A_{ik}}, \\
\delta_{ik} &= \arctan \frac{C_{ik}}{(A_{ik}^2 + B_{ik}^2)^{\frac{1}{2}}}.
\end{aligned}
\tag{6}$$

In the above relations (4) through (6) the elements of translation do not enter the picture. A similar set of relations as per (5) and (6) can be established for the second (XYZ) system.

### 2.1.2 Observation Equations

The mathematical model (4) then, for each  $(i-k)^{th}$  line, yields the following generalized form of observation equations [Uotila, 1967]:

$$\begin{aligned}
&\begin{bmatrix} -1 & 0 & 1 & 0 \\ 0 & -1 & 0 & 1 \end{bmatrix} \begin{bmatrix} v_T \\ v_b \end{bmatrix}_{ik} + \begin{bmatrix} 1 & \sin T_{ik}^{(1)} \tan \delta_{ik}^{(1)} & -\cos T_{ik}^{(1)} \tan \delta_{ik}^{(1)} \\ 0 & \cos T_{ik}^{(1)} & \sin T_{ik}^{(1)} \end{bmatrix}_{ik} \begin{bmatrix} \omega \\ \psi \\ \epsilon \end{bmatrix} \\
&+ \begin{bmatrix} (T_{ik}^{(1)} - T_{ik}^{(2)}) \\ (\delta_{ik}^{(1)} - \delta_{ik}^{(2)}) \end{bmatrix}_{ik} = 0
\end{aligned}
\tag{7}$$

Using the conventional weight matrix  $P$  for the coordinates of points included in the transformation (see section 2.1.3), and the principle of least squares by making  $V'PV$  as minimum, the equation (7) is then solved for correction vector  $(\omega, \psi, \epsilon)$  and for the variance-covariance matrix  $(\Sigma\omega\psi\epsilon)$  of the three parameters.

### 2.1.3 Weights

Using the variance-covariance matrices  $\Sigma X$  and  $\Sigma U$  in respect of  $i^{\text{th}}$  and  $k^{\text{th}}$  points for the XYZ and UVW systems, the variance-covariance matrices  $\Sigma_{\tau\delta}$  for the two systems of coordinates can be computed through propagation of errors [Uotila, 1967].

Two distinct cases would arise here. Firstly, when in addition to correlation between X, Y, Z-coordinates of any point, the correlation between the coordinates of one point to others is also considered. In such a case, the necessary relation will be

$$\left[ \Sigma_{\tau\delta}^{(1)} \right]_{2,2} = G \begin{bmatrix} \Sigma U_i & \Sigma U_{ik} \\ \Sigma U_{ik} & \Sigma U_k \end{bmatrix} G' \quad (8)$$

where

$$G = \begin{bmatrix} \frac{\partial T_{ik}^{(1)}}{\partial U_i} & \frac{\partial T_{ik}^{(1)}}{\partial V_i} & \frac{\partial T_{ik}^{(1)}}{\partial W_i} & \frac{\partial T_{ik}^{(1)}}{\partial U_k} & \frac{\partial T_{ik}^{(1)}}{\partial V_k} & \frac{\partial T_{ik}^{(1)}}{\partial W_k} \\ \frac{\partial \delta_{ik}^{(1)}}{\partial U_i} & \frac{\partial \delta_{ik}^{(1)}}{\partial V_i} & \frac{\partial \delta_{ik}^{(1)}}{\partial W_i} & \frac{\partial \delta_{ik}^{(1)}}{\partial U_k} & \frac{\partial \delta_{ik}^{(1)}}{\partial V_k} & \frac{\partial \delta_{ik}^{(1)}}{\partial W_k} \end{bmatrix},$$

and

$$\frac{\partial T_{ik}}{\partial U_i} = - \frac{\partial T_{ik}}{\partial U_k} = - \frac{\Delta V_{ik}}{\Delta U_{ik}^2 + \Delta V_{ik}^2},$$

$$\frac{\partial T_{ik}}{\partial V_i} = - \frac{\partial T_{ik}}{\partial V_k} = - \frac{\Delta U_{ik}}{\Delta U_{ik}^2 + \Delta V_{ik}^2},$$

$$\frac{\partial T_{ik}}{\partial W_i} = - \frac{\partial T_{ik}}{\partial W_k} = 0,$$

$$\frac{\partial \delta_{ik}}{\partial U_i} = - \frac{\partial \delta_{ik}}{\partial U_k} = \frac{\Delta U_{ik} \Delta W_{ik}}{R_{ik}^{2(1)} \sqrt{\Delta U_{ik}^2 + \Delta V_{ik}^2}},$$

$$\frac{\partial \delta_{ik}}{\partial V_i} = - \frac{\partial \delta_{ik}}{\partial V_k} = \frac{\Delta V_{ik} \Delta W_{ik}}{R_{ik}^{2(1)} \sqrt{\Delta U_{ik}^2 + \Delta V_{ik}^2}},$$

$$\frac{\partial \delta_{ik}}{\partial W_i} = -\frac{\partial \delta_{ik}}{\partial W_k} = -\frac{\sqrt{\Delta U_{ik}^2 + \Delta V_{ik}^2}}{R_{ik}^{(1)}},$$

$$R_{ik}^{(2)} = \Delta U_{ik}^2 + \Delta V_{ik}^2 + \Delta W_{ik}^2$$

Secondly, ignoring the correlations between the coordinates of different points within a system, equation (8) can be modified as under:

$$\left[ \Sigma_{\tau\delta}^{(1)} \right]_{2,2} = G \begin{bmatrix} \Sigma U_i & 0 \\ 0 & \Sigma U_k \end{bmatrix} G' \quad (9)$$

In the equations (8) and (9),  $\Sigma U_i$  and  $\Sigma U_k$  correspond to  $i^{\text{th}}$  and  $k^{\text{th}}$  point of the first system and can be either full ( $3 \times 3$ ) matrices with covariances between the three coordinates of a point, or may contain variances for U, V and W in a diagonal form only. However, in the case of covariances ( $\Sigma U_{ik}$ ) between the points being included, the matrix in equation (8) would be a full ( $6 \times 6$ ).

Obtaining similarly  $\Sigma_{\tau\delta}^{(2)}$ , the combined variance-covariance matrix, to be used with equation (7), is given by:

$$P_{4,4} = \begin{bmatrix} \Sigma_{\tau\delta}^{(2)} & 0 \\ 0 & \Sigma_{\tau\delta}^{(1)} \end{bmatrix} \quad (10)$$

It may be noted here that the matrix P is always in  $2 \times 2$  banded diagonal form.

## 2.2 Determination of Scale Factor

### 2.2.1 Mathematical Model

The scale factor between the systems #1 and #2 would be given as follows:

$$\Delta S_{ik} = \frac{R_{ik}^{(2)}}{R_{ik}^{(1)}} - 1 \quad (11)$$

where  $R_{ik}^{(2)} = (\Delta X_{ik}^2 + \Delta R_{ik}^2 + \Delta Z_{ik}^2)^{\frac{1}{2}}$

$$R_{ik}^{(1)} = (\Delta U_{ik}^2 + \Delta V_{ik}^2 + \Delta W_{ik}^2)^{\frac{1}{2}}$$

### 2.2.2. Weights

Using the variance-covariances matrices  $\Sigma X$  and  $\Sigma U$  for the coordinates of  $i^{\text{th}}$  and  $k^{\text{th}}$  points in the two systems included in the transformation (section 2.1.3), a variance  $\sigma_{\Delta s}^2$  is established for the scale factor through error propagation. Two cases similar to equations (8) and (9) would arise according to the case when full variance-covariance matrix between different points within the system is considered or not.

The matrix G for the scale factor determination is

$$G = \left[ \frac{\partial \Delta s}{\partial U_i} \frac{\partial \Delta s}{\partial V_i} \frac{\partial \Delta s}{\partial W_i} \frac{\partial \Delta s}{\partial U_k} \frac{\partial \Delta s}{\partial V_k} \frac{\partial \Delta s}{\partial W_k} \frac{\partial \Delta s}{\partial X_i} \frac{\partial \Delta s}{\partial Y_i} \frac{\partial \Delta s}{\partial Z_i} \frac{\partial \Delta s}{\partial X_k} \frac{\partial \Delta s}{\partial Y_k} \frac{\partial \Delta s}{\partial Z_k} \right],$$

where

$$\frac{\partial \Delta s}{\partial U_i} = -\frac{\partial \Delta s}{\partial U_k} = \frac{\Delta U_{ik} \cdot R_{ik}^{(2)}}{[R_{ik}^{(1)}]^{3/2}},$$

$$\frac{\partial \Delta s}{\partial V_i} = -\frac{\partial \Delta s}{\partial V_k} = \frac{\Delta V_{ik} \cdot R_{ik}^{(2)}}{[R_{ik}^{(1)}]^{3/2}},$$

$$\frac{\partial \Delta s}{\partial W_i} = -\frac{\partial \Delta s}{\partial W_k} = \frac{\Delta W_{ik} \cdot R_{ik}^{(2)}}{[R_{ik}^{(1)}]^{3/2}},$$

$$\frac{\partial \Delta s}{\partial X_i} = -\frac{\partial \Delta s}{\partial X_k} = -\frac{\Delta X_{ik}}{R_{ik}^{(1)} \cdot R_{ik}^{(2)}},$$

$$\frac{\partial \Delta s}{\partial Y_i} = -\frac{\partial \Delta s}{\partial Y_k} = -\frac{\Delta Y_{ik}}{R_{ik}^{(1)} \cdot R_{ik}^{(2)}},$$

$$\frac{\partial \Delta s}{\partial Z_i} = -\frac{\partial \Delta s}{\partial Z_k} = -\frac{\Delta Z_{ik}}{R_{ik}^{(1)} \cdot R_{ik}^{(2)}}.$$



Hence,

$$\sigma_{\Delta s_{1k}}^2 = G \begin{bmatrix} \Sigma U_1 & \Sigma U_{1k} & 0 \\ \Sigma U_{1k} & \Sigma U_k & \Sigma X_1 - \Sigma X_{1k} \\ 0 & \Sigma X_{1k} & \Sigma X_k \end{bmatrix}_{12} G' \quad (12)$$

where the full  $(12 \times 12)$  matrix would become a  $(3 \times 3)$  banded diagonal matrix in case  $\Sigma U_{1k}$  and  $\Sigma X_{1k}$  are zero, i.e., covariances are not considered. The complete  $(12 \times 12)$  matrix would assume a diagonal pattern when only variances are used for station coordinates.

Using the value of  $\Delta s_{1k}$  and  $\sigma_{\Delta s_{1k}}^2$  from equations (11) and (12), the value for weighted mean and its variance for the transformation under investigation is established as given below [Hirvonen, 1971]:

$$\Delta s_n = \frac{[w_{1k} \cdot \Delta s_{1k}]}{[w_{1k}]} \quad (13)$$

$$\sigma_{\Delta s_n}^2 = \frac{[w_{1k} \cdot (\Delta s_{1k} - \Delta s_n)^2]}{[w_{1k}](n-1)} \quad (14)$$

where

$$w_{1k} = 1/\sigma_{\Delta s_{1k}}^2 \text{ and } [w_{1k}] \text{ denotes the sum of all such weights.}$$

$$n = \text{Total number of scale factor values used in the sample.}$$

### 3. BRIEF DISCUSSION ON THE FORTRAN PROGRAM

Appendix I gives the complete computer program for obtaining the constrained or non-constrained solution for seven parameters. With appropriate coding non-constrained solutions for three parameters ( $\Delta X$ ,  $\Delta Y$  and  $\Delta Z$ ) and scale factor  $\Delta s$  can also be obtained.

The input coordinates can either be Cartesian or geodetic (ellipsoidal) with 35 as the maximum number of points in each system. However, the matrices can easily be re-dimensioned to accomodate more points when required. The

program is self-explanatory with regard to definition of various option codes for input, type of solution and inclusion of correlation data, etc.

The broad basic divisions of the program are as under:

- (a) Main Program: This section takes as input the various options in input/solutions, coordinates of points, rectangular or ellipsoidal, and semimajor axis and flattening of the ellipsoid used, if required. It then prints out the two sets of coordinates used for checking purposes.

The various options of input/solutions have been designated in the program as KCODE e.g., KCODE (1) refers to number of common points involved in the transformation. A complete list with necessary explanatory remarks has been included in the beginning of the program.

- (b) Subroutine "EULERS": This subroutine first reads the variance-covariance matrices of the station coordinates, with or without correlation, and then sets up matrices A, W and P to be used for the solutions of three rotations through direction cosines (equation (7)).

The subroutine writes up the variance-covariance matrices for the coordinates on the disk and stores the estimates for  $\omega, \psi$  and  $\epsilon$ , and their variance-covariance matrix  $[\Sigma\omega\psi\epsilon]$  in the common block for subsequent use.

- (c) Subroutine "SCALE": This subroutine computes the weighted mean value for scale factor  $\Delta s$  and its variance by direct chord comparison independent of other transformation parameters (equations (13) and (14)).
- (d) Subroutine "TFORM": This subroutine solves for a general transformation (equation (3)), utilizing the common block core memory for coordinates of points and variance-covariance matrices from the disk.

The matrix  $M^1$  to be utilized for generating normal equations is computed by calling another subroutine "SETUP".

NOTE: In case the solution is required ONLY for three translation or three translations and scale factor, KCODE (3) is coded as "0" and then subroutine "EULERS" is skipped by the program.

- (e) Subroutine "CSTRNT": This subroutine uses the results of subroutines SCALE and EULERS as constraints with their appropriate statistics and computes for a constrained solution of seven parameters. The results are returned to subroutine TFORM for printout. KCODE (11) refers to the option whether 3 or 4 parameters are to be constrained.
- (f) Subroutine "RESIDU": This subroutine computes the residuals vector V for observations i. e. , the station coordinates used in the program. The residuals are printed station wise for both systems #1 and #2.

In the computer program, the storage mode used for major computation is in vector form for increased flexibility and saving of core storage.

Appendix II gives a typical set of Job Control Cards (JCL).

#### 4. NUMERICAL EXAMPLE

The above transformation models were used to study the relationship between the transformation parameters and obtaining their best estimates by minimizing correlation for the following two reference systems:

- (i) System MPS-7, [Mueller and Whiting, 1972].
- (ii) System NA-9, [Mueller et. al., 1972].

Using the same set of thirty common stations of the above two systems, the following solutions were obtained during the investigation:

Serial Number	Type of Variance-Covariance Matrix Used	7-Parameter General Transformation		
		Unconstrained Solution	Constrained Solution @	
			Constraints: 3 Rotation	Constraints: 3 Rotations and Scale Factor
			(a)	(b)
(i)	Only Variances	✓	✓	✓
(ii)	(3 × 3) Banded Diagonal Variance-Covariance Matrix	✓	✓	✓
(iii)	Full Variance-Covariance Matrix	✓	✓	✓

@Note: The constraints for these solutions (rotations and/or scale factor) with their statistics were computed independently of the translation parameters (subroutine EULERS and SCALE of the Fortran IV program).

Two solutions in full have been appended in the report as specimens in Tables 1 and 2 as under:

Table 1: Sample printout of the solution for three rotations ( $\omega, \psi, \epsilon$ ) and scale factor ( $\Delta s$ ), using full variance-covariance matrix.

Table 2: Sample printout of the constrained seven parameter general solution between NA-9 and MPS-7 with three rotations and

TABLE 1

Sample Printout of the solutions for three rotations as parameters and the scale factor, using full variance-covariance matrix.

TABLE 1

SOLUTION FOR '3' ROTATION PARAMETERS  
 -----  
 (FROM DIRECTION COSINES -- UNITS SECONDS OF ARC)  
 (USING FULL VARIANCE-COVARIANCE MATRIX)

OMEGA

PSI

EPSILON

0.1693791D+00

-0.3520145D-01

-0.2173630D+00

VARIANCE - COVARIANCE MATRIX  
 -----

MD2= 1.36

0.16753861D-02

0.40623287D-03

-0.93767764D-03

0.40623287D-03

0.12317991D-02

-0.48803740D-03

-0.93767764D-03

-0.48803740D-03

0.27191935D-02

COEFFICIENT OF CORRELATION  
 -----

0.10000000D+01

0.28277933D+00

-0.43931501D+00

0.28277933D+00

0.10000000D+01

-0.26666321D+00

-0.43931501D+00

-0.26666321D+00

0.10000000D+01

SOLUTION FOR SCALE FACTOR  
 -----

(FROM CHORD COMPARISON)

SCALE FACTOR  
 (10.D+5)

VARIANCE  
 (10.D+11)

5.16

0.06

TABLE 2

Sample printout of the constrained seven parameters  
general solution, using full variance-covariance matrix  
(case (c)/(iii)).

TABLE 2

SCALE FACTOR AND ROTATION PARAMETERS CONSTRAINED

SOLUTION FOR 3 TRANSLATION, 1 SCALE AND 3 ROTATION PARAMETERS

(USING FULL VARIANCE-COVARIANCE MATRIX)

DX METERS	DY METERS	DZ METERS	DL (10.D+5)	OMEGA SECONDS	PSI SECONDS	EPSILON SECONDS
-45.38	171.94	187.44	5.14	0.17	-0.04	-0.22

VARIANCE - COVARIANCE MATRIX

MO2= 0.84

0.176D+01	0.250D+00	0.453D+00	-0.310D-07	0.126D-06	0.778D-07	-0.852D-07
0.250D+00	0.228D+01	-0.322D-01	0.243D-06	0.551D-07	0.238D-07	-0.124D-06
0.453D+00	-0.322D-01	0.206D+01	-0.149D-06	0.615D-07	0.222D-07	-0.177D-06
-0.310D-07	0.243D-06	-0.149D-06	0.441D-13	-0.325D-17	-0.298D-16	-0.127D-16
0.126D-06	0.551D-07	0.615D-07	-0.325D-17	0.225D-13	0.525D-14	-0.125D-13
0.778D-07	0.238D-07	0.222D-07	-0.298D-16	0.525D-14	0.167D-13	-0.654D-14
-0.852D-07	-0.124D-06	-0.177D-06	-0.127D-16	-0.125D-13	-0.654D-14	0.364D-13

COEFFICIENTS OF CORRELATION

0.100D+01	0.125D+00	0.238D+00	-0.111D+00	0.635D+00	0.454D+00	-0.337D+00
0.125D+00	0.100D+01	-0.149D-01	0.765D+00	0.244D+00	0.122D+00	-0.429D+00
0.238D+00	-0.149D-01	0.100D+01	-0.493D+00	0.286D+00	0.120D+00	-0.648D+00
-0.111D+00	0.765D+00	-0.493D+00	0.100D+01	-0.103D-03	-0.110D-02	-0.317D-03
0.635D+00	0.244D+00	0.286D+00	-0.103D-03	0.100D+01	0.271D+00	-0.436D+00
0.454D+00	0.122D+00	0.120D+00	-0.110D-02	0.271D+00	0.100D+01	-0.265D+00
-0.337D+00	-0.429D+00	-0.648D+00	-0.317D-03	-0.436D+00	-0.265D+00	0.100D+01



scale factor as constraints, using full variance-covariance matrix (case (c)/(iii)).

A summary of the results for cases (a) through (c) and (i) through (iii) are presented in the following tables:

TABLE 3 gives the results for three rotations, as obtained independently of translations and scale factor from direction cosines, for cases (i) through (iii).

TABLE 4 gives the results for the scale factor, as obtained by direct chord comparisons independent of other transformation parameters, for cases (i) through (iii).

TABLE 5 gives the results for the constrained and non-constrained seven parameters general transformation solutions (cases (a) through (c) and (i) through (iii)).

TABLE 6 gives the comparative study of the results for seven parameters general transformation solutions as regards correlation between translations and rotations/scale factor, using different variance-covariance matrices (cases (i) through (iii)).

TABLE 7 gives the comparative study of the results for seven parameters general transformation solutions as regards correlation between translations and rotations/scale factor, using different constraints (cases (a) through (c)).

TABLE 3

Three Rotation Parameters from Direction Cosines

NA-9~MPS-7

	Using Variances Only	Using (3x3) Banded Diagonal Variance- Covariance Matrix	Using full Variance- Covariance Matrix
Case	(i)	(ii)	(iii)
$\omega (")$	$0.17 \pm 0.05$	$0.17 \pm 0.04$	$0.17 \pm 0.04$
$\psi (")$	$0.04 \pm 0.04$	$-0.02 \pm 0.04$	$-0.04 \pm 0.04$
$\epsilon (")$	$-0.20 \pm 0.06$	$-0.24 \pm 0.05$	$-0.22 \pm 0.05$
$\sigma_0^2$	1.15	1.30	1.36

TABLE 4

Scale Factor From Chord Comparison

NA-9~MPS-7

	Using Variances Only	Using (3x3) Banded Diagonal Variance- Covariance Matrix	Using full Variance- Covariance Matrix
Case	(i)	(ii)	(iii)
$\Delta s (\times 10^6)$	$5.46 \pm 0.24$	$5.37 \pm 0.24$	$5.18 \pm 0.24$

TABLE 5

## Seven Parameters General Transformation Solutions

NA-9~MPS-7

	Non-Constrained Solutions				Constrained Solutions						
					Constraints: 3 Rotations						
	Using Variances Only	Using Banded Diagonal Variance-Covariance Matrix	Using Full Variance-Covariance Matrix		Using Variances Only	Using Banded Diagonal Variance-Covariance Matrix	Using Full Variance-Covariance Matrix				
Case	(a)/(i)	(a)/(ii)	(a)/(iii)		(b)/(i)	(b)/(ii)	(b)/(iii)		(c)/(i)	(c)/(ii)	(c)/(iii)
$\Delta X$ (m)	-44.5 $\pm$ 5.2	-44.9 $\pm$ 3.6	-44.9 $\pm$ 3.6		-44.0 $\pm$ 1.7	-44.8 $\pm$ 1.4	-45.0 $\pm$ 1.4		-44.4 $\pm$ 1.7	-45.2 $\pm$ 1.4	-45.4 $\pm$ 1.3
$\Delta Y$ (m)	171.5 $\pm$ 5.1	170.3 $\pm$ 4.7	170.3 $\pm$ 4.7		170.1 $\pm$ 3.8	169.6 $\pm$ 4.0	169.4 $\pm$ 4.0		173.0 $\pm$ 1.7	173.2 $\pm$ 1.5	171.9 $\pm$ 1.5
$\Delta Z$ (m)	190.4 $\pm$ 5.5	190.4 $\pm$ 4.3	190.4 $\pm$ 4.3		188.1 $\pm$ 2.8	189.4 $\pm$ 2.7	189.0 $\pm$ 2.7		186.3 $\pm$ 1.8	187.2 $\pm$ 1.5	187.4 $\pm$ 1.4
$\omega$ (")	0.15 $\pm$ 0.16	0.17 $\pm$ 0.12	0.17 $\pm$ 0.12		0.16 $\pm$ 0.04	0.17 $\pm$ 0.03	0.17 $\pm$ 0.03		0.16 $\pm$ 0.04	0.17 $\pm$ 0.03	0.17 $\pm$ 0.03
$\psi$ (")	0.04 $\pm$ 0.14	-0.03 $\pm$ 0.11	-0.03 $\pm$ 0.11		0.04 $\pm$ 0.04	-0.02 $\pm$ 0.03	-0.04 $\pm$ 0.03		0.04 $\pm$ 0.04	-0.02 $\pm$ 0.03	-0.04 $\pm$ 0.03
$\epsilon$ (")	-0.30 $\pm$ 0.20	-0.28 $\pm$ 0.15	-0.28 $\pm$ 0.15		-0.21 $\pm$ 0.05	-0.24 $\pm$ 0.04	-0.22 $\pm$ 0.04		-0.21 $\pm$ 0.05	-0.24 $\pm$ 0.04	-0.22 $\pm$ 0.04
$\Delta s(\times 10^6)$	4.9 $\pm$ 0.7	4.7 $\pm$ 0.7	4.7 $\pm$ 0.7		4.9 $\pm$ 0.7	4.7 $\pm$ 0.7	4.7 $\pm$ 0.7		5.4 $\pm$ 0.23	5.3 $\pm$ 0.2	5.1 $\pm$ 0.2
$\sigma_0^2$	0.95	0.83	0.83		0.91	0.79	0.79		0.97	0.85	0.84

TABLE 6

Comparative Study of Correlation Coefficients  
Between Transformation Parameters  
 (Using Different Variance-Covariance Matrices)

Case (i): USING VARIANCES ONLY

	Non-Constrained Solution			Constrained Solutions					
				3 Rotations			3 Rotations and Scale Factor		
Case	(a)			(b)			(c)		
Rotations and Scale Factor \ Translations	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$
$\omega$	0.88	0.40	0.43	0.68	0.14	0.22	0.71	0.32	0.35
$\psi$	0.63	0.19	0.13	0.49	0.07	0.08	0.51	0.14	0.13
$\epsilon$	-0.47	-0.67	-0.88	-0.38	-0.23	-0.45	-0.40	-0.51	-0.73
$\Delta s$	-0.10	0.74	-0.40	-0.29	0.95	-0.83	-0.10	0.72	-0.44

Case (ii): USING (3 × 3) BANDED DIAGONAL  
 VARIANCE-COVARIANCE MATRIX

	Non-Constrained Solution			Constrained Solutions					
				3 Rotations			3 Rotations and Scale Factor		
Case	(a)			(b)			(c)		
Rotations and Scale Factor \ Translations	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$
$\omega$	0.83	0.27	0.33	0.58	0.09	0.14	0.62	0.24	0.27
$\psi$	0.54	0.11	0.13	0.38	0.04	0.08	0.40	0.12	0.13
$\epsilon$	-0.45	-0.51	0.80	-0.32	-0.16	-0.34	-0.34	-0.44	-0.66
$\Delta s$	-0.15	0.84	-0.56	-0.36	0.97	-0.89	-0.11	0.76	-0.49

TABLE 6 (Continued)

Case (iii): USING FULL VARIANCE-COVARIANCE MATRIX

	Non-Constrained Solution			Constrained Solutions					
				3 Rotations			3 Rotations and Scale Factor		
Case	(a)			(b)			(c)		
Translations Rotations and Scale Factor	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$
$\omega$	0.83	0.27	0.33	0.60	0.09	0.15	0.64	0.24	0.29
$\psi$	0.54	0.11	0.13	0.43	0.04	0.07	0.45	0.12	0.12
$\epsilon$	-0.45	-0.51	-0.80	-0.32	-0.16	-0.34	-0.34	-0.43	-0.65
$\Delta s$	-0.15	0.84	-0.56	-0.36	0.97	-0.89	-0.11	0.76	-0.49

TABLE 7

Comparative Study of Correlation Coefficients  
Between Transformation Parameters  
 (Using Different Constraints)

Case (a): NON-CONSTRAINED SOLUTION

	Using Variances Only			Using (3x3) Banded Diagonal Variance-Covariance Matrix			Using Full Variance-Covariance Matrix		
Case	(i)			(ii)			(iii)		
Rotations and Scale Factor \ Translations	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$
$\omega$	0.88	0.40	0.43	0.83	0.27	0.33	0.83	0.27	0.33
$\psi$	0.63	0.19	0.13	0.54	0.11	0.13	0.54	0.11	0.13
$\epsilon$	-0.47	-0.67	-0.88	-0.45	-0.51	0.80	-0.45	-0.51	0.80
$\Delta s$	-0.10	0.74	-0.40	-0.15	0.84	-0.56	-0.15	0.84	-0.56

Case (b): CONSTRAINED SOLUTIONS

(CONSTRAINTS: 3 ROTATIONS)

	Using Variances Only			Using (3x3) Banded Diagonal Variance-Covariance Matrix			Using Full Variance-Covariance Matrix		
Case	(i)			(ii)			(iii)		
Rotations and Scale Factor \ Translations	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$
$\omega$	0.68	0.14	0.22	0.58	0.09	0.14	0.60	0.09	0.15
$\psi$	0.49	0.07	0.08	0.38	0.04	0.08	0.43	0.04	0.07
$\epsilon$	-0.38	-0.23	-0.45	-0.32	-0.16	-0.34	-0.32	-0.16	-0.34
$\Delta s$	-0.29	0.95	-0.83	-0.36	0.97	-0.89	-0.36	0.97	-0.89

TABLE 7 (Continued)

Case (c): CONSTRAINED SOLUTIONS  
(CONSTRAINTS: 3 ROTATIONS AND SCALE FACTOR)

	Using Variances Only			Using (3x3) Banded Diagonal Variance-Covariance Matrix			Using Full Variance-Covariance Matrix		
Case	(i)			(ii)			(iii)		
Translations Rotations and Scale Factor	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$
$\omega$	0.71	0.32	0.35	0.62	0.24	0.27	0.64	0.24	0.29
$\psi$	0.51	0.14	0.13	0.40	0.12	0.13	0.45	0.12	0.12
$\epsilon$	-0.40	-0.51	-0.73	-0.34	-0.44	-0.66	-0.34	-0.43	-0.65
$\Delta s$	-0.10	0.72	-0.44	-0.11	0.76	-0.49	-0.11	0.76	-0.49

## 5. CONCLUSIONS

The comparison between different columns of Table 3 shows that the estimates for three rotation parameters remain more or less the same, but that their standard deviations show some improvement as we proceed from column 1 (variances only) to column 3 (full variance-covariance matrix). However, in the case of scale factor (Table 4) the estimates for  $\Delta s$  indicate a definite trend while standard deviation remains constant.

In the case of seven parameters general transformation (Table 5) the comparisons among different columns indicate a definite overall improvement in all parameter estimates. The best estimates were obtained in the solution using full variance-covariance matrix and three rotations ( $\omega, \psi, \epsilon$ ) and scale factor ( $\Delta s$ ) as constraints (column 10). In this case the standard deviations for all the parameters are smaller (or at the most, equal) compared to those in any other column of Table 5.

Further, it is also noticeable that the improvement from a non-constrained solution to a constrained solution, both with three or four constraints, is more significant compared to the improvement from a constrained solution using variances only to a constrained solution using  $(3 \times 3)$  banded diagonal or full variance-covariance matrix. The improvement from the solution using  $(3 \times 3)$  banded diagonal to the solution using full variance-covariance matrix is, however, marginal.

A study of Table 6 indicates in all the three cases an overall improvement in correlation from a non-constrained to a constrained solution with four constraints (three rotations and one scale factor). The improvement in correlation between translations and rotations is quite significant while the same is not reflected between translations and scale factor. However, the improvement pattern from Table 7 is not straightforward. The correlations between translations and rotations show a downward trend from the solutions using variances only to the solutions using full variance-covariance matrix in all the three cases while the correlations between translations and  $\Delta s$  show an upward trend.



## REFERENCES

- Badekas, John (1969). "Investigations Related to the Establishment of a World Geodetic System," Reports of the Department of Geodetic Science, No. 124, The Ohio State University, Columbus.
- Bursa, M. (1966). "Fundamentals of the Theory of Geometric Satellite Geodesy," Travaux de L'Institut Geophysique de L'Academie Teheco-Slovaque des Sciences, No. 241.
- Hirvonen, R. A. (1971). "Adjustment by Least Squares in Geodesy and Photogrammetry," Frederick Ungar Publishing Co.
- Lambeck, K. (1971). "The Relation of Some Geodetic Datums to a Global Geocentric Reference System," Bulletin Géodésique, No. 99, March, 1971.
- Marsh, J. G., B. C. Douglas and S. M. Klosko (1971). "A Unified Set of Tracking Stations Coordinates Derived from Geodetic Satellite Tracking Data," Report No. X-553-71 320, Goddard Space Flight Center, Greenbelt, Maryland.
- Mueller, Ivan I., James P. Reilly and Tomas Soler (1972). "Geodetic Satellite Observation in North America (Solution NA-9)," Reports of the Department of Geodetic Science, No. 187, The Ohio State University, Columbus.
- Mueller, Ivan I. and Marvin C. Whiting (1972). "Free Adjustment of a Geometric Global Satellite Network (Solution MPS-7)," Reports of the Department of Geodetic Science, No. 188, The Ohio State University, Columbus.
- Uotila, Urho A. (1967). "Introduction to Adjustment Computation with Matrices," Department of Geodetic Science, The Ohio State University, Columbus.
- Wolf, H. (1963). "Geometric Connection and Re-orientation of Three-dimensional Triangulation Nets," Bulletin Géodésique, No. 68, June.

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## APPENDIX I

### Fortran IV Program with Subroutines







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      IMPLICIT REAL * 8(A-H , Q-Z)
      REAL      *8 LEMDA,NI,MO2
      DIMENSION XYZ(35,3),RANGLE(4),VROT(4,4),NAME1(3),
2             A(3600),W(1200),P(2400),UVW(35,3),NAME2(3),
3             AA(3,105),BB(3,105),NSTA(35),KSTA(35),KCODE(15)
      COMMON    /WEIGHT/ P
      COMMON    /CODE/ KCODE
      COMMON    /INAME/ NAME1,NAME2
      COMMON    NSTA,KSTA,NN,NM,UVW,XYZ,A,W,KPR,KPARM
      COMMON    /ANGLE/ RANGLE,VROT
      DATA     MINUS/1H-/
      PII       = 3.141592653589793D0
      RHO       = 180.D0/PII
      RHO5      = RHO*3600.D0
      KOUNT     = 1

C
C
C ***** READ IN VARIOUS CODES INVOLVED
C
C
1000 READ      (5, 1) (KCODE(I), I = 1,15), (NAME1(I), I=1,3),
2             (NAME2(I), I=1,3)
      1 FORMAT  (I2,11I1,I2,2I1,3X,3A4,3X,3A4)
      WRITE     (6, 2) (KCODE(I), I = 1,15)
      2 FORMAT  ('1',////////,25X,'KCODE INPUT',//,20X,15I2,/)
      NO       = KCODE(1)
      IF       (KCODE(4).EQ.0.AND.KCODE(5).EQ.0) GO TO 12

C
C ***** READ IN DATA FOR THE FIRST SYSTEM
C
      READ      (5, 3) AE1,F
      3 FORMAT  (2F15.10)
      F        = 1.D0/F
      E2       = 2.D0*F - F*F
      IF       ( KCODE(5) .EQ. 1) GO TO 6

C
C ***** READ IN ELLIPSOIDAL COORDINATES IN DEGREES AND HEIGHT
C
      DO 5 I = 1 , NO
      READ      (5, 4) NSTA(I),PHI,LEMDA,HT
      4 FORMAT  (I4,5X,3F16.9)
      PHI      = PHI / RHO
      LEMDA    = LEMDA / RHO
      WW       = (1.D0-E2 *DSIN(PHI)*DSIN(PHI))*0.5D0
      UVW(I,1)= (AE1/WW+HT)*DCOS(PHI)*DCOS(LEMDA)
      UVW(I,2)= (AE1/WW+HT)*DCOS(PHI)*DSIN(LEMDA)
      UVW(I,3)= (((AE1*(1.D0-E2 ))/WW)+HT)*DSIN(PHI)
      5 CONTINUE
      GO TO 15

C
C
C ***** READ IN ELLIPSOIDAL COORDINATES IN GEOS FORMAT
C
C
      6 DO 11 I = 1 , NO
      READ      (5 , 7) NSTA(I),ISN,IPH,MPH,SPH,ILM,MLM,SLM,HT
      7 FORMAT  (I4,20X,A1,2I3,F8.3,2I3,F8.3,F10.2)
      LEMDA    = (ILM+((MLM+(SLM/60.D0))/60.D0))/RHO

```



```

      IF      (ISN .EQ. MINUS) GO TO 8
      PHI     =  (IPH+((MPH+(SPH/60.00))/60.00))/RHO
      GO TO 10
8     PHI     =  -(IPH+((MPH+(SPH/60.00))/60.00))/RHO
10    WW      =  (1.00-E2*DSIN(PHI)*DSIN(PHI))*0.500
      UVW(I,1) =  (AE1/WW+HT)*DCOS(PHI)*DCOS(LEMDA)
      UVW(I,2) =  (AE1/WW+HT)*DCOS(PHI)*DSIN(LEMDA)
      UVW(I,3) =  (((AE1*(1.00-E2))/WW)+HT)*DSIN(PHI)
11    CONTINUE
      GO TO 15

C
C
C *****      READ IN RECTANGULAR COORDINATES ( U, V, W ) IN METERS
C
C
12    DO 14 I = 1 , NO
      READ    (5, 13) NSTA(I),(UVW(I,J),J=1,3)
13    FORMAT(14,5X,3F16.5)
14    CONTINUE

C
C
C **** READ IN COORDINATES OF THE SECOND SYSTEM
C
C
15    IF      (KCODE(6).EQ.1.OR .KCODE(7).EQ.1) GO TO 20

C
C *****      READ IN RECTANGULAR COORDINATES ( X, Y, Z ) IN METERS
C
C
      DO 18 I = 1 , NO
      READ    (5, 16) KSTA(I),(XYZ(I,J), J=1,3)
16    FORMAT (14,5X,3F16.9)
18    CONTINUE
      GO TO 40
20    READ    (5, 22) AE2,F
22    FORMAT (2F15.10)
      F      =  1.00/F
      E2     =  2.00*F - F*F
      IF      ( KCODE(7) .EQ. 1) GO TO 25

C
C
C *****      READ IN ELLIPSOIDAL COORDINATES IN DEGREES AND HEIGHT
C
C
      DO 24 I = 1 , NO
      READ    (5, 23) KSTA(I),PHI,LEMDA,HT
23    FORMAT (14,5X,3F16.9)
      PHI     =  PHI / RHO
      LEMDA   =  LEMDA / RHO
      WW      =  (1.00-E2 *DSIN(PHI)*DSIN(PHI))*0.500
      XYZ(I,1) =  (AE2/WW+HT)*DCOS(PHI)*DCOS(LEMDA)
      XYZ(I,2) =  (AE2/WW+HT)*DCOS(PHI)*DSIN(LEMDA)
      XYZ(I,3) =  (((AE2*(1.00-E2 ))/WW)+HT)*DSIN(PHI)
24    CONTINUE
      GO TO 40

```

```

C ***** READ IN ELLIPSOIDAL COORDINATES IN GEOS FORMAT
C
C
25 DO 31 I = 1, NO
   READ      (5, 26) KSTA(I), ISN, IPH, MPH, SPH, ILM, MLM, SLM, HT
26 FORMAT    (14, 20X, A1, 2I3, F8.3, 2I3, F8.3, F10.2)
   LEMDA     = (ILM + ((MLM + (SLM/60.00))/60.00))/RHO
   IF (ISN.EQ. MINUS) GO TO 28
   PHI       = (IPH + ((MPH + (SPH/60.00))/60.00))/RHO
   GO TO 30
28 PHI       = -(IPH + ((MPH + (SPH/60.00))/60.00))/RHO
30 WW        = (1.00 - E2 * DSIN(PHI) * DSIN(PHI)) * 0.500
   XYZ(I,1)  = (AE2 / WW + HT) * DCOS(PHI) * DCOS(LEMDA)
   XYZ(I,2)  = (AE2 / WW + HT) * DCOS(PHI) * DSIN(LEMDA)
   XYZ(I,3)  = (((AE2 * (1.00 - E2)) / WW) + HT) * DSIN(PHI)
31 CONTINUE

C
C
C
C **** WRITING OF READ IN DATA FOR THE TWO SYSTEM IN RECTANGULAR COORDINATES
C
C
40 WRITE(6, 42)
42 FORMAT('1', ///, 25X, 'RECTANGULAR COORDINATES FOR FIRST SYSTEM', ///)
   WRITE(6, 43)
43 FORMAT(' ', 13X, 'STN.NO.', 12X, 'U', 13X, 'V', 16X, 'W', /)
   DO 46 I = 1, NO
   WRITE(6, 44) NSTA(I), (UVW(I,J), J=1,3)
44 FORMAT(' ', 13X, I5, F20.4, 2F16.4, (14X, I5, F20.4, 2F16.4))
46 CONTINUE
   WRITE(6, 50)
50 FORMAT('1', ///, 25X, 'RECTANGULAR COORDINATES FOR SECOND SYSTEM', /)
   WRITE(6, 52)
52 FORMAT(' ', 13X, 'STN.NO.', 12X, 'X', 13X, 'Y', 16X, 'Z', /)
   DO 60 I = 1, NO
   WRITE(6, 58) KSTA(I), (XYZ(I,J), J=1,3)
58 FORMAT(' ', 13X, I5, F20.4, 2F16.4, (14X, I5, F20.4, 2F16.4))
60 CONTINUE

C
C
C **** SEPARATING THE TYPE OF SOLUTION REQUIRED
C
C
   KPARM     = KCODE(11)
   IF (KCODE(8).NE. 1) GO TO 62
   KPR       = 1
   GO TO 75
62 IF (KCODE(9).NE. 1) GO TO 64
   KPR       = 2
   GO TO 75
64 KPR       = 3
   IF (KCODE(10).EQ.1.AND.KCODE(12).EQ.1) KPR = 2
75 NM        = NO - 1
   NN        = NO * NM
   NNN       = 3 * NO
   IF (KCODE(14).EQ. 0) GO TO 85
   CALL FULERS (NO, NNN, AA, BB)

```

```
      IF      (KCODE(14).EQ.1.AND.KCODE(2).EQ.3) GO TO 95
85  CALL TFORM (NO,NNN)
      IF (KOUNT .EQ. KCODE(13)) GO TO 95
      KOUNT   =   KOUNT + 1
      GO TO 1000
95  STOP
     END
```



```

      B(2,3) = 0.00
      NS     = NN/2
      B(2,4) = 1.00
      DO 1 I = 1, 2
      DO 1 J = 1, 4
      BT(J,I) = B(I,J)
1  CONTINUE
      DO 2 I = 1, 4
      DO 2 J = 1, 4
      PR(I,J) = 0.00
2  CONTINUE
      IF      (KCODE(8).EQ.1.OR.KCODE(9).EQ.1) GO TO 10

C
C
C *****<<***** *
C
C *****
C          FULL VARIANCE-COVARIANCE CASE
C
C *****<<***** *
C
C
C ***** READING IN VARIANCE-COVARIANCES FOR 'FIRST SYSTEM'
C
C
C
      JK      = 1
      DO 6 I = 1, NNN
      JL      = JK + NNN - I
      READ    (5, 3) (QUVW(J), J = JK,JL)
3  FORMAT    (8F10.4)
      DO 4 L = LL, 3
      P1(LL,L) = QUVW(JK+L-LL)
4  P1(L,LL) = P1(LL,L)
      WRITE   (1) (P1(LL,M), M = 1, 3)
      LL     = LL + 1
      IF      (LL.EQ. 4) LL = 1
6  JK      = JL + 1
      REWIND  1

C
C
C ***** READING IN VARIANCE-COVARIANCES FOR 'SECOND SYSTEM'
C
C
C
      LL      = 1
      JK      = 1
      DO 9 I = 1, NNN
      JL      = JK + NNN - I
      READ    (5, 7) (QXYZ(J), J = JK,JL)
7  FORMAT    (8F10.4)
      DO 8 L = LL, 3
      P2(LL,L) = QXYZ(JK+L-LL)
8  P2(L,LL) = P2(LL,L)
      WRITE   (2) (P2(LL,M), M = 1, 3)

```



```

      KM      = KK + 2
      IF      (KCODE(8) .EQ. 1) GO TO 20
C
C
C **** VARIANCE - COVARIANCE MATRIX IN 3X3 BANDED FORM
C
      DO 19 J = 1, 3
      READ      (5,18) (BB(J,K), K=KK,KM)
18  FORMAT (3F5.2)
19  WRITE(2) (BB(J,K), K=KK,KM)
      GO TO 23
C
C
C
C **** VARIANCE - COVARIANCE MATRIX IN DIAGONAL FORM (ONLY VARIANCES)
C
      DO 21 J = 1, 3
      DO 21 K = KK,KM
21  BB(J,K) = 0.00
      READ      (5,15) (BB(K,(K+KK-1)), K = 1,3)
      DO 22 J = 1, 3
22  WRITE(2) (BB(J,K), K=KK,KM)
23  CONTINUE
      REWIND 2
C
C
C *****<*****
C **** FORMING MATRICES 'A', 'W', AND 'P' FOR THE ENTIRE SYSTEM      **** *
C **** BY COMPUTING DIRECTION COSINES FOR EACH LINE BETWEEN          **** *
C **** ANY ONE SET OF TWO GIVEN POINTS.                               **** *
C                                                                           *
C *****<*****
C
24  MKR      = 1
      KMT      = 1
      MK      = 1
      INDEX(1) = 1
      MM1      = NNN + 1
      DO 25 I = 1, NO
25  INV(I) = 3*I - 1
      DO 26 I = 1, NM
      DO 26 J = 1, 6
      DO 26 K = 1, 6
      P1(J,K) = 0.00
      P2(J,K) = 0.00
26  CONTINUE
      IF      (KCODE(10).EQ. 1) GO TO 28
      DO 27 J = 1, 3
      DO 27 L = 1, 3
      LL      = (I-1) * 3 + L
      P1(J,L) = AA(J,LL)
      P2(J,L) = BB(J,LL)

```

```

27 CONTINUE
GO TO 32
28 LL = INDEX(I)
DO 30 J = 1, 3
DO 29 L = J, 3
LLL = LL + L - J
P1(J,L) = QUVW(LLL)
29 P2(J,L) = QXYZ(LLL)
MM1 = MM1 - 1
30 LL = LL + MM1
32 JJ = I + 1
INDEX(JJ) = LL
MM2 = MM1
DO 50 K = JJ, NO
IF (KCODE(8).EQ.1.OR.KCODE(9).EQ.1) GO TO 43
LL = INDEX(K)
DO 34 J = 4, 6
DO 33 L = J, 6
LLL = LL + L - J
P1(J,L) = QUVW(LLL)
33 P2(J,L) = QXYZ(LLL)
MM2 = MM2 - 1
34 LL = LL + MM2
KP = K + 1
INDEX(KP) = LL
III = INDEX(I) + INV(K-I)
IF (KCODE(12).EQ.1) GO TO 41
DO 38 J = 1, 3
DO 36 L = 4, 6
LLL = III + L - 3
P1(J,L) = QUVW(LLL)
36 P2(J,L) = QXYZ(LLL)
38 III = III + (NNN - (3*(I-1)) - J)
41 DO 42 J = 1, 6
DO 42 L = 1, 6
P1(L,J) = P1(J,L)
42 P2(L,J) = P2(J,L)
GO TO 45
43 DO 44 L = 4, 6
JKL = L - 3
DO 44 M = 4, 6
KLM = (K-2)*3 + M
P1(L,M) = AA(JKL,KLM)
P2(L,M) = BB(JKL,KLM)
44 CONTINUE
45 KSM = MKR + NN
KMS = MKR + (2*NN)

```

```

C
C
C **** COMPUTING DIRECTION COSINES FOR FIRST SYSTEM
C
C

```

```

DA1 = UVW(K,1) - UVW(I,1)
DB1 = UVW(K,2) - UVW(I,2)
DC1 = UVW(K,3) - UVW(I,3)
RIK1 = DSQRT(DA1*DA1+DB1*DB1+DC1*DC1)
AIK1 = DA1/RIK1
BIK1 = DB1/RIK1

```



```

      CIK1   = DC1/RIK1
      TIK1   = -DATAN2(BIK1,AIK1)
      IF      (TIK1.LT.0.)  TIK1 =(360.00+TIK1*RHO)/RHO
      AB1     = DSQRT(AIK1*AIK1+BIK1*BIK1)
      DIK1    = DATAN2(CIK1,AB1)

C
C
C **** COMPUTING DIRECTION COSINES FOR SECOND SYSTEM
C
C
      DA2     = XYZ(K,1) - XYZ(1,1)
      DB2     = XYZ(K,2) - XYZ(1,2)
      DC2     = XYZ(K,3) - XYZ(1,3)
      RIK2    = DSQRT(DA2*DA2+DB2*DB2+DC2*DC2)
      AIK2    = DA2/RIK2
      BIK2    = DB2/RIK2
      CIK2    = DC2/RIK2
      TIK2    = -DATAN2(BIK2,AIK2)
      IF      (TIK2.LT.0.)  TIK2 =(360.00+TIK2*RHO)/RHO
      AB2     = DSQRT(AIK2*AIK2+BIK2*BIK2)
      DIK2    = DATAN2(CIK2,AB2)

C
C
C **** SETTING UP MATRICES 'A' AND 'W' -- COMMON TO ALL SOLUTION
C
C
      A(MKR)  = 1.00
      A(MKR+1)= 0.00
      A(KSM)  = DSIN(TIK2)*DTAN(DIK2)
      A(KSM+1)= DCOS(TIK2)
      A(KMS)  = -DCOS(TIK2)*DTAN(DIK2)
      A(KMS+1)= DSIN(TIK2)
      W(MKR)  = TIK1 - TIK2
      W(MKR+1)= DIK1 - DIK2

C
C *****
C
C **** FORMING VAR-COVARIANCE MATRIX FOR 'TIK' AND 'DIK' *****
C **** THROUGH PROPOGATION OF ERRORS -- WHERE 'TIK' AND *****
C **** ARE GEODETIC HOUR ANGLE AND DECLINATION. *****
C
C *****
C
C ****
C
C **** FIRST SYSTEM ****
C
      DAB1    = DA1*DA1+DB1*DB1
      DBA     = DSQRT(DAB1)
      G(1,1)  = -DB1/DAB1
      G(1,2)  = DA1/DAB1
      G(1,3)  = 0.00
      G(1,4)  = -G(1,1)

```

```

G(1,5) = -G(1,2)
G(1,6) = 0.00
G(2,1) = DA1*DC1/(DBA*RIK1*RIK1)
G(2,2) = DB1*DC1/(DBA*RIK1*RIK1)
G(2,3) = -DBA/(RIK1*RIK1)
G(2,4) = -G(2,1)
G(2,5) = -G(2,2)
G(2,6) = -G(2,3)
DO 46 L = 1, 2
DO 46 M = 1, 6
GT(M,L) = G(L,M)
46 CONTINUE
CALL DGMPRD(G,P1,GP,2,6,6)
CALL DGMPRD(GP,GT,PP,2,6,2)

```

C  
C  
C  
C  
C  
C  
C

\*\*\*\*

SECOND SYSTEM

\*\*\*\* \*

```

DAB2 = DA2*DA2+DB2*DB2
DAB = DSQRT(DAB2)
G(1,1) = -DB2/DAB2
G(1,2) = DA2/DAB2
G(1,3) = 0.00
G(1,4) = -G(1,1)
G(1,5) = -G(1,2)
G(1,6) = 0.00
G(2,1) = DA2*DC2 / (DAB*RIK2*RIK2)
G(2,2) = DB2*DC2 / (DAB*RIK2*RIK2)
G(2,3) = -DAB/(RIK2*RIK2)
G(2,4) = -G(2,1)
G(2,5) = -G(2,2)
G(2,6) = -G(2,3)
DO 47 L = 1, 2
DO 47 M = 1, 6
GT(M,L) = G(L,M)
47 CONTINUE
CALL DGMPRD(G,P2,GP,2,6,6)
CALL DGMPRD(GP,GT,PQ,2,6,2)

```

C  
C  
C  
C  
C  
C  
C

\*\*\*\* FORMING MATRIX 'MI' FOR THE COMBINED SYSTEM

```

DO 48 L = 1, 2
J = L + 2
DO 48 M = 1, 2
N = M + 2
PR(L,M) = PQ(L,M)
PR(J,N) = PP(L,M)
48 CONTINUE
CALL DGMPRD(B,PR,BS,2,4,4)
CALL DGMPRD(BS,BT,PP,2,4,2)
CALL DMINV(PP,2,DT,KX,KY)

```



```

      DO 85 J = 1 , 3
      NI(J,I) = 0.00
      DO 85 K = 1 , NN
      III      = (J-1)*NN + K
95  NI(J,I) = NI(J,I) + A(III)*W(K)
88  CONTINUE
      REWIND      3
      IF          (KCODE(11) .EQ. 3) GO TO 89
      N7(1,1) = WT
89  DO 91 I = 2 , 4
      DO 91 J = 2 , 4
91  NZ(I,J) = NI(I-1,J-1)
      CALL DMINV(NI,3,DEF,KQ,LQ)
C
C
C *****<<*****
C **** COMPUTING SOLUTION VECTOR ' DX ' FOR 3 ROTATION PARAMETERS **** *
C *****<<*****
C
      READ(4)      (W(I), I=1 , NN)
      REWIND      4
      DO 92 J = 1 , 3
      U(J) = 0.00
      DO 92 I = 1 , NN
      KKK      = (J-1)*NN + I
      U(J) = U(J) - A(KKK)*W(I)
92  CONTINUE
      CALL DGMPRD(NI,U,DX,3,3,1)
      DO 95 I = 1 , 3
      JK      = (I-1)*NN + 1
      JM      = JK + NN - 1
95  READ(3)      (A(J), J= JK , JM)
      REWIND      3
C
C
C
C **** COMPUTING VARIANCE OF UNIT WEIGHT ' MD2 '
C
      DO 96 I = 1 , NN
      W(I) = 0.00
      DO 96 J = 1 , 3
      K      = (J-1)*NN + I
      W(I) = W(I) - A(K)*DX(J)
96  CONTINUE
      READ(4)      (A(I), I= 1 , NN)
      REWIND      4
      DO 97 K = 1 , NN
      W(K) = W(K) - A(K)
97  CONTINUE
      MMM      = 0
      DO 98 K = 1 , NN

```

```

      A(K)      = 0.00
      L1       = ((K-1)/2)*2 + K
      L2       = L1 + 2
      DO 98 L = L1, L2, 2
      MMM      = ((L-1)/2) + 1
98      A(K)    = A(K) + P(L)*W(MMM)
      READ(4)   (W(I), I = 1, NN)
      REWIND    4
      VPV      = 0.00
      DO 99 K = 1, NN
99      VPV    = VPV - A(K)*W(K)
      MD2      = VPV/(NN - 3)

C
C
C
C **** COMPUTING VARIANCE- COVARIANCE MATRIX 'VAR'
C
C
C
      DO 100 I = 1, 3
      DO 100 J = 1, 3
      VAR(I,J) = MD2*RHOS*RHOS*NI(I,J)
100      CONTINUE
      DO 105 I = 1, 3
105      DX(I) = DX(I)*RHOS

C
C
C **** COMPUTING COEFFICIENTS OF CO-RELATIONS FOR PARAMETERS
C
C
C
      DO 110 I = 1, 3
      IF (I.EQ.3) GO TO 107
      JJ = I + 1
      DO 106 J = JJ, 3
      NI(I,J) = VAR(I,J)/(DSQRT(VAR(I,I))*DSQRT(VAR(J,J)))
106      NI(J,I) = NI(I,J)
107      NI(I,I) = 1.00
110      CONTINUE

C
C *****
C
C **** WRITING OF FINAL SOLUTION VECTOR AND VARIANCE-COVARIANCE MATRIX
C
C
C *****
C
      WRITE(6,6025)
6025  FORMAT('1',///)
      WRITE(6,6028) (NAME1(I),I=1,3),(NAME2(I),I=1,3)
6028  FORMAT(' ',5X,3A4,'-TO-',3A4,/,
26X,'*****'//)
      WRITE(6,6030)
6030  FORMAT(' ',30X,'SOLUTION FOR '3' ROTATION PARAMETERS',/,
231X,'-----',/,
325X,'(FROM DIRECTION COSINES -- UNITS SECONDS OF ARC)',/,
      GO TO (112,114,116), KPR
112  WRITE(6,6031)

```

```

6031 FORMAT(' ',37X,'(USING VARIANCES ONLY)',//)
      GO TO 120
114  WRITE(6,6032)
6032 FORMAT(' ',21X,
2'(USING 3X3 BANDED DIAGONAL VARIANCE-COVARIANCE MATRIX)',//)
      GO TO 120
116  WRITE(6,6033)
6033 FORMAT(' ',29X,'(USING FULL VARIANCE-COVARIANCE MATRIX)',//)
120  WRITE(6,6035)
6035 FORMAT(' ',20X,'OMEGA',19X,'PSI',20X,'EPSILON',//)
      WRITE(6,6040)(DX(I), I=1,3)
6040 FORMAT(' ', 5X,3D24.7,//)
      WRITE(6,6045)
6045 FORMAT(' ',32X,'VARIANCE - COVARIANCE MATRIX',/,
233X,'-----',//)
      WRITE(6,6048) MO2
6048 FORMAT(' ',17X,'MO2=',F6.2,//)
      WRITE(6,6050)((VAR(I,J), J=1,3), I=1,3)
6050 FORMAT(' ', 3X,3D25.8,/( 4X,3D25.8,//)
      WRITE(6,6075)
6075 FORMAT(' ',33X,'COEFFICIENT OF CORRELATION',/,
234X,'-----',//)
      WRITE(6,6085)((NI(I,J),J=1,3),I=1,3)
6085 FORMAT(' ', 3X,3D25.8,/( 4X,3D25.8,//)
      IF (KCODE(11) .EQ. 3) GO TO 150
      WRITE (6,7000)
7000 FORMAT(' ',//,34X,'SOLUTION FOR SCALE FACTOR',/,
234X,'-----',//,
335X,'(FROM CHORD COMPARISON)',//)
      WRITE (6,7004)
7004 FORMAT(' ',20X,'SCALE FACTOR',27X,'VARIANCE',/,
223X,'(10.D+5)',29X,'(10.D+11)',//)
      WRITE (6,7010) S , VSF
7010 FORMAT(' ',20X,F8.2,30X,F7.2,//)
150  KCODE(11) = 4
      RETURN
      END

```



```

      A(1)      = 0.00
12  CONTINUE
      DO 15 I = 1, NQ
      KKK      = (3*I-2)
      LLL      = KKK+NQ+1
      MMM      = LLL+NQ+1
      A(KKK)   = 1.00
      A(LLS)   = 1.00
      A(MMM)   = 1.00
C
C
C **** SETTING UP MATRIX 'W' WHICH IS COMMON TO ALL SOLUTION
C
C
      W(KKK)   = (UVW(I,1)-XYZ(I,1))
      W(KKK+1) = (UVW(I,2)-XYZ(I,2))
      W(KKK+2) = (UVW(I,3)-XYZ(I,3))
15  CONTINUE
      IF (KCODE(2) .NE. 3) GO TO 50
C
C
C **** SOLUTION FOR 3 TRANSLATION PARAMETERS
C
C
      N = 3
      ICASF = 1
      GO TO 81
C
C
C
C **** SOLUTION FOR 3 TRANSLATION AND 1 SCALE PARAMETERS
C
C
C
50  N = 4
      DO 60 I = 1, NQ
      KKK      = 3*(NQ+1)-2
      A(KKK)   = UVW(I,1)
      A(KKK+1) = UVW(I,2)
      A(KKK+2) = UVW(I,3)
60  CONTINUE
      IF (KCODE(2) .NE. 4) GO TO 70
      ICASF = 2
      GO TO 81
C
C
C
C **** SOLUTION FOR 3 TRANSLATION, 1 SCALE AND 3 ROTATION PARAMETERS
C
C
C
70  N = 7
      ICASF = 3
      DO 80 I = 1, NQ
      KKK      = 4*NQ+(3*I-2)

```



```

      LLL      = KKK + NQ
      MMM      = LLL + NQ + 1
      A(KKK)   = UVW(I,2)
      A(KKK+1) = -UVW(I,1)
      A(LLL)   = -UVW(I,3)
      A(LLL+2) = UVW(I,1)
      A(MMM)   = UVW(I,3)
      A(MMM+1) = -UVW(I,2)
80    CONTINUE
81    DO 85 I = 1 , N
      KKK      = (I-1)*NQ+1
      LLL      = KKK+NQ-1
      WRITE(3) (A(J), J=KKK,LLL)
85    CONTINUE
      REWIND   3
      WRITE(4) (W(I), I=1,NQ)
      REWIND   4

C *****
C *****
C **** FORMING NORMAL EQUATIONS -- MATRICES 'N' AND 'U'
C *****
C *****
C *****
100  CALL SETUP (NQ,NQ,IPARA)
      DO 118 I = 1 , N
      READ(3) (W(J), J=1,NQ)
      K1      = (I-1)*NQ+1
      K2      = K1+NQ-1
      MMM      = 0
      DO 116 K= K1, K2
      A(K)     = 0.00
      L1      = (((K-K1)/3)*3)+1
      L2      = L1 + 2
      DO 116 L = L1 , L2
      MMM      = MMM + 1
116  A(K)      = A(K) + W(L)*MI(MMM)
118  CONTINUE
      REWIND   3
      DO 120 I = 1 , N
      READ(3) (W(L), L= 1,NQ)
      JK      = (I-1)*N+1
      JL      = JK+N-1
      DO 119 J = JK,JL
      NI(J)   = 0.00
      DO 119 K = 1 , NQ
      I1      = (J-JK)*NQ + K
119  NI(J)     = NI(J) + A(I1)*W(K)
120  CONTINUE
      REWIND   3
      DO 121 I = 1 , N
      DO 121 J = 1 , N
      K      = (I-1)*N + J
121  SIGMAX(I,J) = NI(K)
      READ(4) (W(I), I= 1,NQ)
      REWIND   4
      DO 122 J=1 , N

```

```

      U(J) = 0.00
      DO 122 I=1 , NQ
      KKK = (J-1)*NQ+1
      U(J) = U(J) - A(KKK)*W(I)
122  CONTINUE
C
C *****<<*****
C
C **** COMPUTING SOLUTION VECTOR 'DX' FOR TRANSFORMATION PARAMETERS
C
C *****<<*****
C
      CALL DMINV(NI,N,DT,LT,MT)
      CALL DARRAY(1,N,N,7,7,NI,VR)
      CALL DGMPRD(NI,U,DX,N,N,1)
      DO 123 I = 1 , N
      JK = (I-1)*NQ + 1
      JM = JK + NQ -1
123  READ(3) (A(J),J=JK,JM)
      REWIND 3
C
C
C **** COMPUTING VARIANCE OF UNIT WEIGHT 'MO2'
C
C
      DO 125 I = 1 , NQ
      W(I) = 0.00
      DO 125 J = 1 , N
      KZX = (J-1)*NQ+1
      W(I) = W(I) -A(KZX)*DX(J)
125  CONTINUE
      READ(4) (A(I), I= 1, NQ)
      REWIND 4
      DO 126 K = 1, NQ
      W(K) = W(K)-A(K)
126  CONTINUE
      MMM = 0
      DO 128 K = 1 , NQ
      A(K) = 0.00
      L1 = ((K-1)/3)*6 + K
      L2 = L1 + 6
      DO 128 L = L1,L2,3
      MMM = ((L-1) /3) +1
128  A(K) = A(K) +MI(L)*W(MMM)
      CALL RESIDU (NQ,NNN)
      READ(4) (W(I),I= 1,NQ)
      REWIND 4
      VPV = 0.00
      DO 130 K = 1,NQ
130  VPV = VPV - A(K)*W(K)
      MG2 = VPV/(NQ-N)
C
C
C **** COMPUTING VARIANCE-COVARIANCE MATRIX 'VAR'
C
C
      DO 122 I = 1, N

```

```

      DO 132 J = 1, N
      VAR(I,J) = MD2*VR(I,J)
132  CONTINUE
      IF (KCODE(2) .EQ. 3) GO TO 140
      DX(4) = DX(4) * 10.05
      IF (KCODE(2) .EQ. 4) GO TO 140
      DO 135 I = 5, 7
      DX(I) = DX(I) * RHOS
135  CONTINUE
C
C
C
C **** COMPUTING COEFFICIENTS OF CORRELATIONS FOR PARAMETERS
C
C
C
140  DO 145 I = 1, N
      IF (I.EQ.N) GO TO 144
      JJ = I + 1
      DO 142 J = JJ, N
      VR(I,J) = VAR(I,J)/(DSQRT(VAR(I,I))*DSQRT(VAR(J,J)))
142  VR(J,I) = VR(I,J)
144  VR(I,I) = 1.00
145  CONTINUE
200  WRITE(6,250)
250  FORMAT('1',//)
      WRITE(6, 300) (NAME1(I),I=1,3), (NAME2(I),I=1,3)
300  FORMAT(' ',5X,3A4,'-TO-',3A4,/,
26X,'*****'//)
      GO TO (500,600,700), ICASE
C
C
C
C *****<<*****
C
C
C **** WRITING OF FINAL SOLUTION VECTOR AND VARIANCE-COVARIANCE MATRIX
C
C
C
C *****<<*****
C
C
500  WRITE(6,6025)
6025  FORMAT(' ',//)
      WRITE(6,6030)
6030  FORMAT(' ',21X,'SOLUTION FOR 3 TRANSLATION PARAMETERS',/,
232X,'(UNITS - METERS)',//)
      GO TO (512,514,516), KPR
512  WRITE(6,6032)
6032  FORMAT(' ',29X,'(USING VARIANCES ONLY)',//)
      GO TO 520
514  WRITE(6,6034)
6034  FORMAT(' ',15X,
2'(USING 3X3 BANDED DIAGONAL VARIANCE-COVARIANCE MATRIX)',//)
      GO TO 520
516  WRITE(6,6036)

```

```

6036 FORMAT(' ',22X,'(USING FULL VARIANCE-COVARIANCE MATRIX)',//)
520 WRITE(6,6038)
6038 FORMAT(' ',16X,'DX',20X,'DY',22X,'DZ',//)
WRITE(6,6040)(DX(I), I=1,3)
6040 FORMAT(' ', 1X,3D23.8,////////)
WRITE(6,6045)
6045 FORMAT(' ',26X,'VARIANCE - COVARIANCE MATRIX',//)
WRITE(6,6048) MD2
6048 FORMAT(' ',14X,'MD2=',F6.2,//)
WRITE(6,6050) ((VAR(I,J), J=1,3), I=1,3)
6050 FORMAT(' ', 1X,3D23.8,/( 2X,3D23.8,/)
WRITE(6,6075)
6075 FORMAT(' ',//,27X,'COEFFICIENTS OF CORRELATION',////)
WRITE(6,6085)((VR(I,J), J=1,N), I=1,N)
6085 FORMAT(' ', 1X,3D23.8,/( 2X,3D23.8,/)
GO TO 1000
600 WRITE(6,6500)
6500 FORMAT(' ',////////)
WRITE(6,6510)
6510 FORMAT(' ',17X,'SOLUTION FOR 3 TRANSLATION AND 1 SCALE PARAMETERS'
2,/,34X,'(UNITS - METERS)',////)
GO TO (612,614,616), KPR
612 WRITE(6,6512)
6512 FORMAT(' ',29X,'(USING VARIANCES ONLY)',//)
GO TO 620
614 WRITE(6,6514)
6514 FORMAT(' ',19X,
2,'(USING 3X3 BANDED DIAGONAL VARIANCE-COVARIANCE MATRIX)',//)
GO TO 620
616 WRITE(6,6516)
6516 FORMAT(' ',22X,'(USING FULL VARIANCE-COVARIANCE MATRIX)',//)
620 WRITE(6,6520)
6520 FORMAT(' ', 6X,'DX',22X,'DY',23X,'DZ',22X,'DL',//)
WRITE(6,6550)(DX(I), I=1,4)
6550 FORMAT(' ',D15.8,3D24.8,////////)
WRITE(6,6600)
6600 FORMAT(' ',26X,'VARIANCE - COVARIANCE MATRIX',//)
WRITE(6,6625) MD2
6625 FORMAT(' ', 8X,'MD2=',F6.2,//)
WRITE(6,6650) ((VAR(I,J), J=1,4), I=1,4)
6650 FORMAT(' ', 1X,4D20.8,/( 2X,4D20.8,/)
WRITE(6,6675)
6675 FORMAT(' ',//,27X,'COEFFICIENTS OF CORRELATION',////)
WRITE(6,6685)((VR(I,J), J=1,N), I=1,N)
6685 FORMAT(' ', 1X,4D20.8,/( 2X,4D20.8,/)
GO TO 1000
700 GO TO ( 710,705) , KOUNT
705 IF (KPARM .EQ. 4) GO TO 708
WRITE (6,7002)
7002 FORMAT(' ',28X,'ROTATION PARAMETERS CONSTRAINED',/,
229X,'-----',//)
GO TO 710
708 WRITE(6,7005)
7005 FORMAT(' ',20X,'SCALE FACTOR AND ROTATION PARAMETERS CONSTRAINED',
2/,21X,'-----',//)
710 WRITE(6,7010)
7010 FORMAT(' ',13X,'SOLUTION FOR 3 TRANSLATION, 1 SCALE AND 3 ROTATION
2 PARAMETERS',/,14X,'-----')

```

```

3,T58,'-----',/)
GO TO (712,714,716), KPR
712 WRITE(6,7012)
7012 FORMAT(' ',34X,'(USING VARIANCES ONLY)',/)
GO TO 720
714 WRITE(6,7014)
7014 FORMAT(' ',16X,
2'(USING 3X3 BANDED DIAGONAL VARIANCE-COVARIANCE MATRIX)',/)
GO TO 720
716 WRITE(6,7016)
7016 FORMAT(' ',24X,'(USING FULL VARIANCE-COVARIANCE MATRIX)',/)
720 WRITE(6,7020)
7020 FORMAT(' ',16X,'DX', 6X,'DY', 6X,'DZ', 7X,'DL', 5X,'OMEGA',
2T 59,'PSI', 4X,'EPSILON',/,
315X,'METERS', 2X,'METERS', 2X,'METERS',1X,'(10.0+5)',1X,'SECONDS',
4T57,'SECONDS', 2X,'SECONDS',/)
WRITE(6,7030) DX
7030 FORMAT(' ',12X,F7.2,2F8.2,F8.2,F9.2,T55,F8.2,F9.2,/)
WRITE(6,7040)
7040 FORMAT('O',28X,'VARIANCE - COVARIANCE MATRIX',/)
WRITE(6,7045) MQ2
7045 FORMAT(' ',10X,'MQ2=',F6.2,/)
WRITE(6,7050) ((VAR(I,J), J=1,7), I = 1,7)
7050 FORMAT(' ',2X,7D11.3,/(3X,7D11.3,/)
WRITE(6,7075)
7075 FORMAT(' ',/, 29X,'COEFFICIENTS OF CORRELATION',/)
WRITE(6,7085)((VR(I,J), J=1,N), I=1,N)
7085 FORMAT(' ', 2X,7D11.3,/( 3X,7D11.3,/)
IF(IC.EQ.0) GO TO 1000
WRITE (6,7090)
7090 FORMAT ('1',////,36X,'RESIDUALS V',/,36X,'-----',///,
212X,'FIRST SYSTEM',33X,'SECOND SYSTEM',/)
KSM = NNN + 1
KMR = NNN - 1 +KSM
WRITE (6,8000) (A(I), I = KSM,KMR)
8000 FORMAT(' ',4X,3F8.3,22X,3F8.3,/(5X,3F8.3,22X,3F8.3))
IF (KCODE(3).EQ. 0) GO TO 1000

```

```

C
C *****<<*****
C
C
C
C ***** OBTAINING CONSTRAINED SOLUTION FOR ROTATION PARAMETERS *****
C
C
C *****<<*****
C
C

```

```

C
CALL CSTRNT(N,NQ,IC,U,CN,CNT,TT,ZP)
KCODE(3) = 0
DO 725 I = 1 , 7
DX(I) = XD(I)
DO 725 J = 1 , 7
VAR(I,J) = SIGMAX(I,J)
725 CONTINUE
DO 750 I = 1,N
IF(1.EQ.N) GO TO 740

```

```

      JJ = I + 1
      DO 735 J = JJ , N
      VR(I,J) = VAR(I,J)/(DSQRT(VAR(I,I))*DSQRT(VAR(J,J)))
735  VR(J,I) = VR(I,J)
740  VR(I,I) = 1.00
750  CONTINUE
      KOUNT = 2
      MQ2 = SQ2
      GO TO 200
1000 RETURN
      END

```



```

      CALL          DGMPRD (H1,H,WS,1,12,1)
C *****
C *****
C *****
C *****
C *****
      WS           = 1.00/WS
      WI(N)        = WS
      SFI          = R2/R1 - 1
      DL(N)        = SFI
      SF           = SF + SFI *WS
      SW           = SW + WS
      S            = SF/SW
C *****
C *****
C *****
C *****
C *****
      FINDING VARIANCE FOR THE WEIGHTED MEAN OF THE SCALE FACTOR
C *****
C *****
      IF           (N.NE.NO) GO TO 500
      PVV          = 0.00
      DO 50 K      = 1 , NO
      VI(K)        = ((S-DL(K))*2)*WI(K)
50  PVV           = PVV + VI(K)
      VSF          = PVV/(SW*(NO-1))
      S            = S * 10.05
      WT           = 1.00 / VSF
500  RETURN
      END

```





```

C
C *****<*****
C
C **** SOLVE FOR EFFECTS OF CONSTRAINTS ON THE SOLUTION VECTOR 'DX'
C **** OBTAINED FROM NON-CONSTRAINT SOLUTION
C
C *****<*****
C
      DO 520 I= 1 , IC
      DO 520 J= 1,N
      CNT(J,I)= CN(I,J)
520  CONTINUE
      CALL MTPY(CNT,ZP,N,IC,IC,TT)
      CALL MTPY(TT,CN,N,IC,N,GG)
      DO 522 I = 1 , N
      DO 522 J = 1 , N
522  GG(I,J) = SIGMAX(I,J) + GG(I,J)
      CALL DMINV(GG,N,DTT,LM,MM)
      CALL MTPY(TT,WC,N,IC,1,WX)
      DO 525 I= 1 , N
      WS(I) = (WS(I) - WX(I))
525  CONTINUE
      CALL MTPY(GG,WS,N,N,1,XD)
C
C **** COMPUTE NEW VARIANCE OF UNIT WEIGHT AND
C **** NEW VARIANCE - COVARIANCE MATRIX
C
      CALL MTPY(CN,XD,IC,N,1,KC)
      DO 535 I = 1 , IC
535  KC(I) = -KC(I)-WC(I)
      CALL MTPY(PZ,KC,IC,IC,1,DX)
      SUM = 0.0
      DO 540 I= 1, IC
      SUM = SUM + DX(I) * WC(I)
540  CONTINUE
      PVV = VPV - SUM
      SD2 = PVV/(NN-N+IC)
      DO 550 I= 1 , N
      DO 550 J= 1 , N
      SIGMAX(I,J) = SD2*GG(I,J)
550  CONTINUE
      XD(4) = XD(4) * 10.05
      DO 560 I = 5 , 7
      XD(I) = XD(I) * RHOS
560  CONTINUE
1000 RETURN
      END

```



```

      IF      (KCODE(8) .EQ. 1) GO TO 54
      DO 40 L = 1 , NO
      DO 39 J = 1 , 3
      READ(5,38) (PI(J,K), K=1,3)
38  FORMAT(3F5.2)
39  WRITE (2)    (PI(J,K) , K = 1 , 3)
40  CONTINUE
      DO 52 M = 1 , NO
      DO 44 J = 4 , 6
      READ(5,42) (PI(J,K), K= 4, 6)
42  FORMAT(3F5.2)
44  CONTINUE
      DO 45 I = 1 , 3
      DO 45 J = 1 , 3
45  PK(I,J) = PI(I+3,J+3)
      DO 50 I = 1 , 3
50  WRITE(1) (PK(I,J), J=1,3)
52  CONTINUE
      REWIND 1
      REWIND 2
      GO TO 65
54  DO 58 M = 1 , NO
      READ (5,55) (PI(I,I) , I= 1,3)
55  FORMAT (3F10.2)
      DO 56 I = 1 , 3
56  WRITE (2) (PI(I,J), J=1,3)
58  CONTINUE
      DO 64 M = 1 , NO
      READ (5,55) (PI(I,I) , I= 4,6)
      DO 60 J = 1 , 3
      DO 60 K = 1 , 3
60  PK(J,K) = PI(J+3,K+3)
      DO 62 I = 1 , 3
62  WRITE(1) (PK(I,J), J = 1,3)
64  CONTINUE
      REWIND 1
      REWIND 2
65  DO 100 I = 1 , NO
      KMS = (I-1)*9 + 1

```

C  
C  
C  
C  
C  
C  
C  
C  
C  
C

```

C **** READ IN VARIANCE - COVARIANCE MATRIX AS BLOCK DIAGONALS
C **** OF (6,6) MATRICES FOR EACH POINT USED IN TRANSFORMATION.
C **** MATRIX 'PI' IS BUILT UP POINTWISE - FIRST (3,3) BLOCK
C **** REFERS TO SECOND COORDINATE SYSTEM AND SECOND (3,3) BLOCK
C **** THEN CORRESPONDS TO FIRST COORDINATE SYSTEM.

```

```

      DO 70 J = 1 , 3
      READ(2) (PI(J,K), K= 1,3)
70  CONTINUE
      DO 74 L = 4 , 6
      READ(1) (PI(L,M), M=4,6)
74  CONTINUE
      CALL MTPY(B,PI,3,6,6,XK)
      CALL MTPY(XK,BT,3,6,3,XM)
      CALL DMINV(XM,3,DET,LM,MM)
      MINK(KMS ) = XM(1,1)

```

```
MINK(KMS+1) = XM(2,1)
MINK(KMS+2) = XM(3,1)
MINK(KMS+3) = XM(1,2)
MINK(KMS+4) = XM(2,2)
MINK(KMS+5) = XM(3,2)
MINK(KMS+6) = XM(1,3)
MINK(KMS+7) = XM(2,3)
MINK(KMS+8) = XM(3,3)
100 CONTINUE
   RFWIND 1
   RFWIND 2
   RETURN
END
```



```

CALL DGMPRD (PI,BT,BS,6,6,3)
C *****
C *****<<<<<<<<<*****<<<<<<<<<*****
C *****
C ***** COMPUTING RESIDUALS *****
C *****
C *****<<<<<<<<<*****<<<<<<<<<*****
C *****
      DO 15 K = 1 , 6
        KK = JJ + K
        A(KK) = O.DO
        KM = (I-1) * 3
      DO 15 L = 1 , 3
        KM = KM + 1
15    A(KK) = A(KK) + BS(K,L) * A(KM)
      DO 20 L = 1 , 3
        LL = JJ + L
        KM = LL + 3
        W(L) = A(LL)
        A(LL) = A(KM)
20    A(KM) = W(L)
25 CONTINUE
REWIND 1
REWIND 2
RETURN
END
```







## **APPENDIX II**

### **Job Control Cards**

## APPENDIX II

```
//      (2500,100),CLASS=C
//STEP1 EXEC PROC=FORTRAN,PARM='MAP,ID',TIME.CMP=(0,30)
//CMP.SYSIN DD *
```

### FORTRAN PROGRAM DECK.

```
/*
//STEP2 EXEC PROC=RUNFORT,PARM.LKED='OVLY,LIST,MAP',TIME.LKED=(0,20),
//      TIME.GO=(3,10),REGION.GO=252K
//LKED.SYSLIB DD DSNAME=SYS1.FORTLIB,DISP=SHR
//              DD DSNAME=SYS2.FORTSSP,DISP=SHR
//LKED.SYSLIN DD DSNAME=*.STEP1.CMP.SYSLIN,DISP=(OLD,DELETE)
// DD *
//      OVERLAY      ALPHA
//      INSERT       EULERS,SCALE
//      OVERLAY      BETA
//      INSERT       TFORM,RESIDU,MTPY,SETUP,CSTRNT,DARRAY
/*
//GO.FT01F001 DD  UNIT=SYSDA,SPACE=(CYL,(1,1)),DISP=(NEW,DELETE),
//              DCB=(RECFM=VBS,LRECL=600,BLKSIZE=604)
//GO.FT02F001 DD  UNIT=SYSDA,SPACE=(CYL,(1,1)),DISP=(NEW,DELETE),
//              DCB=(RECFM=VBS,LRECL=600,BLKSIZE=604)
//GO.FT03F001 DD  UNIT=SYSDA,SPACE=(CYL,(1,1)),DISP=(NEW,DELETE),
//              DCB=(RECFM=VBS,LRECL=600,BLKSIZE=604)
//GO.FT04F001 DD  UNIT=SYSDA,SPACE=(CYL,(1,1)),DISP=(NEW,DELETE),
//              DCB=(RECFM=VBS,LRECL=600,BLKSIZE=604)
//GO.FT07F001 DD  SYSOUT=B
//GO.SYSIN DD *
```

### DATA DECK

```
/*
//
```